

α, β : parametersGood conductors: $\frac{\sigma}{\omega \epsilon} \gg 1$

$$\alpha \approx \beta \approx \sqrt{\frac{\omega \mu \sigma}{2}}$$

$$\eta_c: \text{complex impedance} = \sqrt{\frac{\mu}{\epsilon}} \left(1 - j \frac{\sigma}{\omega \epsilon} \right)^{-1/2} = \sqrt{\frac{\mu}{\epsilon}} (-j)^{1/2} \left(\frac{\sigma}{\omega \epsilon} \right)^{-1/2}$$

$$(-j) = e^{3\pi j/2} \Rightarrow (-j)^{1/2} = e^{3\pi j/4} \quad \downarrow \text{ } \pi/4$$

$$(-j)^{-1/2} = \frac{1}{(-j)^{1/2}} = e^{-3\pi j/4} = \frac{1}{\sqrt{2}} (1+j)$$

$$\eta_c = \sqrt{\frac{\mu}{\epsilon}} \frac{\epsilon \omega}{\sigma} \frac{1}{\sqrt{2}} (1+j) = \sqrt{\frac{\omega \mu}{2 \sigma}} (1+j)$$

Power Propagation IN A WAVE.

Poynting vector (Electromagnetic power density)

For cultural purposes:

$$\vec{F} = q \vec{E} + q \vec{u} \times \vec{B}$$

$$dW = \vec{F} \cdot d\vec{l} \\ = q \vec{E} \cdot d\vec{l} + q d\vec{l} \cdot (\vec{u} \times \vec{B})$$

$$u = \frac{d\vec{l}}{dt} \therefore (\vec{u} \times \vec{B}) \text{ is } \perp \text{ to } d\vec{l} \Rightarrow d\vec{l} \cdot (\vec{u} \times \vec{B}) = 0$$

$$\therefore dW = q \vec{E} \cdot d\vec{l}$$

$$\frac{1}{q} dW = \vec{E} \cdot d\vec{l} = dV$$

$$\text{For } N \text{ particles: } \frac{dW}{dt} \overset{\text{power}}{=} N q \vec{E} \cdot \frac{d\vec{l}}{dt} = N q \vec{E} \cdot \vec{u} = \vec{E} \cdot (N q \vec{u})$$

$$\frac{dW}{dt} = \vec{E} \cdot \vec{J}_c$$

\vec{J}_c
cond.
current
density

$$\vec{E} = \begin{bmatrix} V \\ m \end{bmatrix}, \quad \vec{J}_c = \begin{bmatrix} I \\ m^2 \end{bmatrix}$$

$$\vec{\nabla} \times \vec{H} = \vec{J}_c + \frac{\partial \vec{D}}{\partial t} \rightarrow \vec{J}_c = \vec{\nabla} \times \vec{H} - \frac{\partial \vec{D}}{\partial t}$$

$$\frac{\partial w}{\partial t} = \vec{E} \cdot (\vec{\nabla} \times \vec{H}) - \vec{E} \cdot \left(\frac{\partial \vec{D}}{\partial t} \right)$$

$$\vec{\nabla} \cdot (\vec{A} \times \vec{B}) = \vec{B} \cdot (\vec{\nabla} \times \vec{A}) - \vec{A} \cdot (\vec{\nabla} \times \vec{B}) \quad \leftarrow \text{identity}$$

$$\vec{E} \cdot (\vec{\nabla} \times \vec{H}) = \vec{H} \cdot (\vec{\nabla} \times \vec{E}) + \vec{\nabla} \cdot (\vec{H} \times \vec{E})$$

$$\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$\frac{dw}{dt} = \vec{E} \cdot \vec{J}_c = -\vec{H} \cdot \left(\frac{\partial \vec{B}}{\partial t} \right) - \vec{\nabla} \cdot (\vec{E} \times \vec{H}) - \vec{E} \cdot \left(\frac{\partial \vec{D}}{\partial t} \right)$$

$$\vec{B} = \mu \vec{H}$$

$$\vec{D} = \epsilon \vec{E}$$

$$\Rightarrow \frac{dw}{dt} = \vec{E} \cdot \vec{J}_c = -\frac{\mu}{2} \frac{\partial}{\partial t} (\vec{H} \cdot \vec{H}) - \frac{1}{2} \epsilon \frac{\partial}{\partial t} (\vec{E} \cdot \vec{E}) - \vec{\nabla} \cdot (\vec{E} \times \vec{H})$$

Integrate over volume

$$\int_V (\vec{E} \cdot \vec{J}_c) dV = - \int_V (\vec{\nabla} \cdot (\vec{E} \times \vec{H})) dV - \frac{\partial}{\partial t} \int_V \left(\frac{\mu}{2} (\vec{H} \cdot \vec{H}) + \frac{\epsilon}{2} (\vec{E} \cdot \vec{E}) \right) dV$$

power dissipated in the volume

$$-\int_S (\vec{E} \times \vec{H}) \cdot d\vec{s}$$

flux of energy through the surface that bounds the volume.

$$\vec{E} \times \vec{H} = \vec{P} \quad \text{Poynting vector}$$

↳ power density radiated by the fields.

\vec{P} describes the instantaneous power density carried by the wave

→ Specialisation to plane waves:

For a plane wave travelling along \hat{n} ($\vec{k} = k\hat{n}$)

$$\vec{H}_s = \frac{1}{\eta_c} \hat{n} \times \vec{E}_s \quad \vec{E}_s = \vec{H}_s \times \hat{n}$$

$$\hat{n} = \frac{\vec{E}_s \times \vec{H}_s}{\eta_c} \rightarrow \vec{P} \text{ is along } \hat{n}$$

EXAMPLE:

Steady current I_c through a cylindrical resistor, radius b and length l . The conductivity of the resistor is σ .

$$\vec{J}_c = \hat{z} \cdot \frac{I_c}{\pi b^2}, \quad \vec{J}_c = \sigma \vec{E} \Rightarrow \vec{E} = \hat{z} \cdot \frac{I_c}{\pi b^2 \sigma}$$

$\sigma \neq \infty$
since
conductor is
not perfect.

$$\vec{H} = \frac{I_c}{2\pi b} \hat{\phi}$$

$$\vec{P} = \vec{E} \times \vec{H} = (\hat{z} \times \hat{\phi}) \cdot \frac{I_c^2}{2\pi^2 b^3 \sigma} = -\hat{r} \cdot \frac{I_c^2}{2\pi^2 b^3 \sigma}$$

$$- \int \vec{P} \cdot d\vec{s} : \text{total power flow.}$$

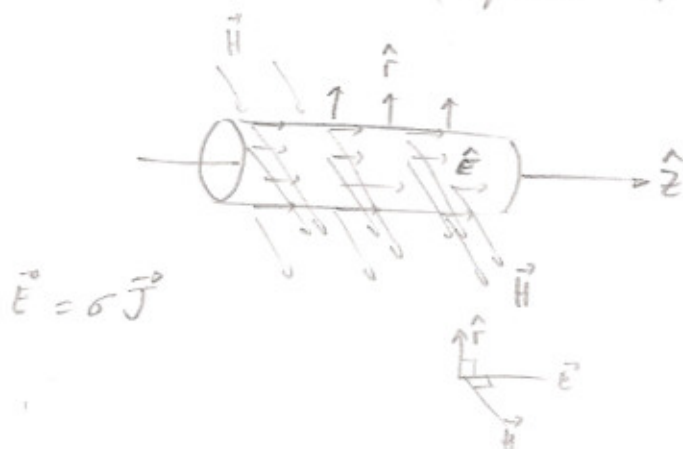
$d\vec{s}$: surface element along \hat{r}

Total power flowing into resistor from the source of \vec{E}, \vec{H} is

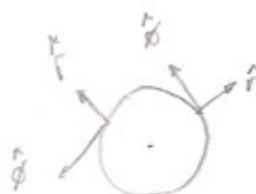
$$\left(\frac{I_c^2}{2\pi^2 b^3 \sigma} \right) \times (2\pi b l) = I_c^2 \frac{l}{\pi b^2 \sigma} = I_c^2 R$$

(regular multiplication)

(R for cylinder
length l
radius b .)



$$\vec{E} = \sigma \vec{J}$$



power that heats
resistor.

$\vec{P} = \vec{E} \times \vec{H}$ is the instantaneous power density

time-averaged \vec{P} or \vec{P}_{avg} or $\langle \vec{P} \rangle$

$$\vec{E}(z,t) = \text{Re} \{ \vec{E}_s e^{j\omega t} \}$$

\vec{E}_s is complex but along \hat{x} .

$$\vec{E}_s = \hat{x} \text{Re} \{ E_{re} + j E_{im} \}$$

$$\vec{H}_s = \hat{y} \left(\frac{E_{re} + j E_{im}}{\eta_c} \right)$$

$$\begin{aligned} \vec{E}(z,t) &= \hat{x} \text{Re} \{ (E_{re} + j E_{im}) (\cos \omega t + j \sin \omega t) \} \\ &= \hat{x} \text{Re} \{ E_{re} \cos \omega t - E_{im} \sin \omega t + j(\dots) \} \end{aligned}$$

$$\vec{E}(z,t) = \hat{x} (E_{re} \cos \omega t - E_{im} \sin \omega t)$$

$$\vec{H}(z,t) = \hat{y} \text{Re} \left\{ \left(\frac{E_{re} + j E_{im}}{\eta_c} \right) \cdot e^{j\omega t} \right\}$$

$$\frac{E_r + j E_i}{\eta_c} = H_r + j H_i \quad (H_r \neq \frac{E_r}{\eta_c})$$

$$\vec{H}(z,t) = \hat{y} (H_{re} \cos \omega t - H_{im} \sin \omega t)$$

$$\vec{P} = (\vec{E} \times \vec{H}) = (\hat{x} \times \hat{y}) \cdot [E_{re} H_{re} \cos^2 \omega t + E_{im} H_{im} \sin^2 \omega t - (E_{re} H_{im} + E_{im} H_{re}) (\cos \omega t \sin \omega t)]$$

Taking time average:

$$\langle \vec{P} \rangle = \frac{1}{T} \int_0^T \vec{P} dt$$

$$\Rightarrow \cos^2 \omega t \rightarrow \frac{1}{2}, \quad \sin^2 \omega t \rightarrow \frac{1}{2}, \quad \sin \omega t \cos \omega t = 0$$

$$\langle \vec{P} \rangle = \hat{z} \frac{1}{2} [E_{re} H_{re} + E_{im} H_{im}] = \frac{1}{2} \text{Re} \{ \vec{E}_s \times \vec{H}_s^* \} \quad (\text{can be verified by direct substitution})$$

$$\rightarrow \boxed{\langle P \rangle = \frac{1}{2} \text{Re} \{ \vec{E}_s \times \vec{H}_s^* \}}$$

Note: $\vec{E}_s = \hat{x} e^{-\alpha z} e^{-j\beta z} E_{ox}$, E_{ox} is real

$$\vec{H}_s = \hat{y} e^{-\alpha z} e^{-j\beta z} \frac{E_{ox}}{\eta_c}$$

Write $\eta_c = |\eta_c| e^{j\theta_\eta}$

$$\vec{H}_s^* = \hat{y} e^{-\alpha z} e^{j\beta z} \frac{E_{ox}}{|\eta_c|} e^{j\theta_\eta}$$

$$\vec{E}_s \times \vec{H}_s^* = (\hat{x} \times \hat{y}) e^{-2\alpha z} \frac{E_{ox}^2}{|\eta_c|} e^{j\theta_\eta}$$

$$\langle \vec{P} \rangle = \frac{1}{2} \cdot \text{Re} \{ \vec{E}_s \times \vec{H}_s^* \} = \hat{z} \frac{1}{2} e^{-2\alpha z} \frac{E_{ox}^2}{|\eta_c|} \cos \theta_\eta$$